

High-efficiency electrochemical methane conversion using Fe_2O_3 -based catalysts assisted by thermochemical active oxygen

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ABSTRACT

Direct methane-alcohol conversion is urgently needed not only for efficient use of methane but also for a sustainable environment. Here, we present hybrid electrochemical methane oxidation with thermochemical generation of active oxygen by employing an Fe_2O_3 -based catalyst with a CO_2 oxygen source. A mechanistic study, including an electrochemical analysis, elucidates the reaction pathway in which the CO_2 activates methane by supplying O^* through thermal dissociation over the Fe_2O_3 catalyst, while an electrochemical potential applied to the Fe_2O_3 catalyst promotes the subsequent methane-ethanol conversion. We demonstrate that doping the catalyst with oxophilic Zr into the catalyst enhances ethanol conversion by stabilizing the hydroxyl-containing intermediates. In room-temperature electrochemical methane conversion, we achieve an ethanol production rate of 1677 $\mu\text{mol/g}_{\text{cat}}/\text{hr}$ (the total production rate for oxygenates is 1831 $\mu\text{mol/g}_{\text{cat}}/\text{hr}$) with a selectivity of 91 % and an 87 % Faraday efficiency conversion.

1. Introduction

The demand for conversion of methane into high value-added chemicals is surging with the abundant supply from shale gas development [1,2]. Conversion of methane to alcohol is advantageous not only in terms of storage/transportation but also in that alcohol can be directly used as a liquid fuel [3]. Since direct conversion of methane to alcohol is difficult due to the high C–H binding energy of methane (439 kJ/mol) with low electron affinity [4–7], commercialized methane-alcohol conversion adopts the route of first decomposing methane (high-temperature reforming, typically >1100 K) at high temperature to produce syngas and then synthesizing alcohol through multistep indirect conversion [8–10]. However, the multistep conversion process including such high-temperature reforming always suffers from economic issues [8–10]. Therefore, for direct methane-alcohol conversion, advanced thermochemical catalysts such as Fe- or Cu-based zeolites (e.g., Fe-ZSM-5, FeCu-ZSM-5, Cu-mordenite) have been extensively explored [11,12]. Specifically, these catalysts mimic the metal-oxo active site of methane monooxygenase that converts methane to methanol at room temperature [13]. Nevertheless, the catalytic process still adopts a multistep process with varying temperature [14,15]. The

process typically consists of activation of the metal-zeolite catalyst by an oxidant (473–773 K), methane oxidation on the metal-oxo site of the catalyst (398–473 K), and extraction of methanol with steam/solvent (473 K). Recently, continuous methane-methanol conversion at a constant temperature over a Cu-zeolite catalyst has been demonstrated, but the conversion rate is extremely low, 0.001 % [16].

Electrocatalytic liquid-phase methane conversion is emerging as a continuous multistep methane-alcohol direct conversion process under mild conditions [17,18]. Specifically, electrocatalytic conversion exhibits distinct features for each step of a catalytic process: catalyst activation, methane oxidation, and product extraction. First, catalyst activation, which is the formation of active atomic oxygen on the catalyst surface, is continuously achieved by electrochemically oxidizing water ($\text{H}_2\text{O} \rightarrow \text{OH}^* \rightarrow \text{O}^*$); this process overlaps with the oxygen evolution reaction (OER) [19,20]. Then, catalytic conversion is controlled by simply adjusting the applied potential [21]. Finally, the electrolyte solution environment allows the immediate extraction of highly soluble alcohol products and the consequent suppression of deep oxidation processes [22,23]. Previously, Singh and coworkers suggested high electrochemical methane oxidation in transition metal oxides such as TiO_2 with high methane binding energy induced by a low Madelung

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potential [24]. Zheng and coworkers performed room temperature electrochemical methane–ethanol conversion with an ethanol production rate of 789 $\mu\text{mol/g}_{\text{cat}}/\text{hr}$ (85 % selectivity) on a Rh/ZnO nanosheet catalyst [25]. Sun and coworkers demonstrated electrochemical methane–ethanol conversion over NiO/Ni catalysts with a production rate of 25 $\mu\text{mol/g}_{\text{cat}}/\text{hr}$ (87 % selectivity) [26]. Nevertheless, the benefits of electrocatalysis have not been fully realized. The biggest hurdle is that the formation of stable O^{*} is difficult under anodic potential as O^{*} is prone to being scavenged by the OER [24]; this issue also occurs with the introduction of a separate oxidant. Besides, highly active methane oxidation catalysts are characterized by weak oxygen binding, so they are likely to exhibit fast OERs [17,19]. Indeed, previous studies on electrochemical methane oxidation with a bimetallic Cu₂O₃/TiO₂ catalyst and a Mg-MOF-74 catalyst reported low Faraday efficiencies (FEs) of 6 % and 10.9 %, respectively, which may be associated with fast OERs [24,27]. Therefore, exploring electrocatalytic reactions with stable O^{*} formation is pursued for highly productive electrochemical methane conversion.

In this study, we present electrochemical methane–ethanol conversion using an Fe₂O₃-based catalyst with a CO₃²⁻ oxygen source (Fig. 1a). Although Fe₂O₃ is applicable as a catalyst for the thermochemically complete oxidation of methane and as a photoelectrochemical water splitting catalyst [28,29], it has yet to be applied to electrochemical

methane conversion processes. The CO₃²⁻ oxygen source has been utilized; however, the usefulness of CO₃²⁻ has not been fully elucidated through mechanistic analysis [30,31]. In this study, our density functional theory (DFT) calculations and experiments reveal that the generation of O^{*} by the dissociative adsorption of CO₃²⁻ on the Fe₂O₃ catalyst occurs thermochemically, avoiding the OER. In addition, we identify a favorable reaction pathway for methane–ethanol conversion; this solution involves a methanol deprotonation process that becomes more endothermic under anodic potentials. Furthermore, we present the promotion of methane–ethanol conversion by Zr doping. Under room-temperature electrochemical methane conversion conditions, we achieve highly selective methane–ethanol conversion with Fe₂O₃-based catalysts. The Zr-doped Fe₂O₃ catalyst attains an ethanol production rate of 1677 $\mu\text{mol/g}_{\text{cat}}/\text{hr}$ ((the total production rate for oxygenates is 1831 $\mu\text{mol/g}_{\text{cat}}/\text{hr}$) with a selectivity reaching 91 %; the Faraday efficiency (FE) for this ethanol conversion process approaches 87 %. This value exceeds the production rate for the partial oxidation of methane resulting from existing electrocatalysts, photocatalysts and liquid-phase heterogeneous catalysts.

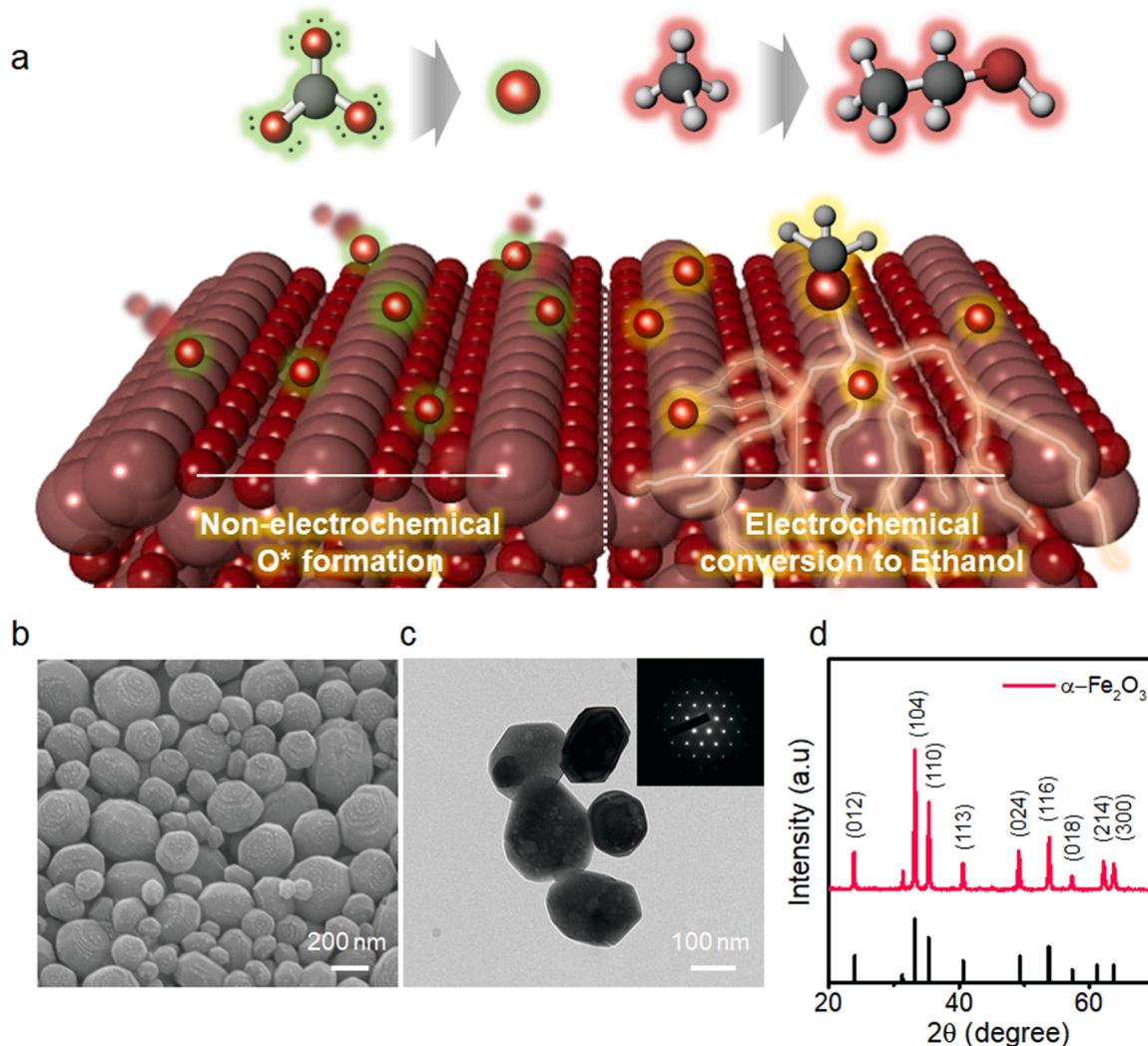


Fig. 1. Material analysis of the Fe₂O₃ catalyst. (a) Schematic diagram of electrochemical oxidation of methane to ethanol assisted by thermochemical generation of active oxygen. (b) Scanning electron microscopy (SEM) and (c) transmission electron microscopy (TEM) images of Fe₂O₃ catalyst nanoparticles. The inset image is the SAED pattern. (d) XRD pattern of the Fe₂O₃ catalyst. (Reference: JCPDS 33 – 0664 for α -Fe₂O₃).

2. Experimental

2.1. Preparation of $\alpha\text{-Fe}_2\text{O}_3$ catalyst

The $\alpha\text{-Fe}_2\text{O}_3$ catalyst was obtained by reacting 0.03 M Iron(III) nitrate nonahydrate and 0.06 M NaCl and 0.2 g poly(N-vinylpyrrolidone) (K-30) were dissolved in mixed solvents of 15 mL DI water and 15 mL ethanol under magnetic stirring. For zirconium doping, calculated amount of Zirconium(IV) oxynitrate hydrate was added to the previously prepared mixed solution to obtain the 0.01, 0.05 and 0.1 wt % Zr-doped Fe_2O_3 . The mixed solution was loaded into a 100 mL Teflon autoclave sealed to 433 K and kept at this temperature for 12 h. The synthesized particles were thoroughly washed with ethanol. Thereafter, the particle was heat treated at 1073 K for 6 h.

2.2. Electrochemical analysis and methane-conversion reaction

The measurement of current versus voltage sweep utilizes a three-electrode system exploiting $\alpha\text{-Fe}_2\text{O}_3$ catalyst-coated glassy carbon as the working electrode, Pt as the counter electrode, and a saturated calomel electrode (SCE) as the reference electrode, using a potentiostat (was recorded using a Versastat, Ametek); The scan rate was 0.02 V/s. The electrolyte contains 0.5 M Na_2CO_3 , where the Na_2CO_3 acts as an oxidizing agent. The dissolution of methane in the electrolyte is obtained by purging the electrolyte with methane at a rate of 30 mL/min for about 30 min before the reaction. The $\alpha\text{-Fe}_2\text{O}_3$ catalyst coated on graphite foil were applied as catalyst electrodes; The coating is obtained by casting a solution of the particles dispersed in Nafion-dissolved ethanol solution (1 % (v/v)) followed by drying in an oven at 373 K for 24 h. The conversion reaction is carried out in a gas-tight reactor (450 mL); The area of the catalyst electrode is typically 10 cm^2 . An electrolyte of 0.5 M Na_2CO_3 is applied. For isotopically-labeled reactions, $^{13}\text{CH}_4$ was purchased from Sigma-Aldrich (99 %, 99 atom % ^{13}C). ^{18}O -labeled carbonate was synthesized by reacting H_2^{18}O (200 μL , 9.1 mmol, 98 % ^{18}O) with tetraethyl orthocarbonate (5 mL, 23.8 mmol) and toluenesulfonic acid (dehydrated, 1.5 mg) for several minutes. It was then dried and reacted with 500 mM sodium methoxide solution (at 385 K for 30 hrs).

2.3. Characterization

The scanning electron microscope (SEM) was recorded using a JSM-7800F (JEOL). The transmission electron microscope (TEM) was recorded using a JEM-ARM200F (JEOL); The microscope was equipped with a spherical aberration corrector in the condenser lens (probe corrector). The high-angle annular dark field-scanning TEM (HAADF-STEM) was conducted by using a JEM-ARM200F (JEOL) microscope at an acceleration voltage of 200 kV. The EDS mapping was recorded using Oxford Instruments X-Max SDD. The XRD was recorded using a Rigaku miniflex-2005G303 X-ray diffractometer (Cu K α radiation at 20 kV and 10 mA) in the 2 theta range of 20–70°. The XPS was analyzed by using a Leybold photoelectron spectroscopy (Al Ka monochromatic beam). ^{13}C NMR is recorded using an Avance III HD 400 FT NMR instrument (Bruker Bio-spin). The measurement is calibrated with a signal of 3-(trimethylsilyl)-1-propane sulfonic acid sodium salt (DSS) at $\delta = 0.0$ ppm. The proton high-power decoupling field strength was 11.7 G (5.0 μs long 90° ^1H pulses). The contact time was 4 ms at the Hartmann-Hahn matching condition 50 kHz, and the scan delay time was 3 s. The ^{13}C chemical shift of the product was analyzed for accuracy of ± 0.5 ppm. Tetramethylsilane (TMS) was applied as an external standard. The ^{13}C chemical shift of the product was analyzed with an accuracy of ± 0.5 ppm; Tetramethylsilane (TMS) was applied as an external standard. Gas chromatography (GC) was obtained using gas chromatography (7820 A, Agilent Technologies, USA) using a flame ionization detector (FID). A PoraPLOT Q column was used, the samples were injected with an airtight syringe, and the injection temperature was 523 K. For the FID a

flow of 300 mL/min Ar, 40 mL/min H_2 fuel and 25 mL/min N_2 make-up was applied. Oven temperature conditions are 2 min at 313 K, 353 K (20 K/min) and 503 K (30 K/min). Gas chromatography-mass spectra are measured by gas chromatography (GC-MS, 7890B-5977A, Agilent Technologies, USA) equipped with a mass selective detector MSD 5975 (electron impact ionization, EI, 70 eV, Agilent Technologies). Fused silica capillaries (DB-WAX, 0.5 μm thick poly(ethylene glycol) coating, Agilent Technologies, USA) are utilized. The injection temperature is 250 degrees. The carrier gas is helium (1 mL/min, 99.999 %) and the dilution ratio is 10:1 (sample: He). Oven temperature conditions are 5 min at 313 K, 4 K/min (373 K), and 3 min at 513 K (20 K/min).

3. Results and discussion

3.1. Catalyst synthesis

Fe_2O_3 nanoparticles are synthesized by the hydrothermal reduction of an iron(III) nitrate precursor[32]. The Fe_2O_3 particles have polyhedral shapes with diameters in the range of 50–300 nm (Fig. 1b and S1). The Brunauer–Emmett–Teller (BET) surface area is 176 m^2/g (Fig. S2). The selected area electron diffraction (SAED) pattern shows sharp diffraction spots, indicating high crystallization (Fig. 1c). The X-ray diffraction (XRD) pattern exhibits peaks corresponding to $\alpha\text{-Fe}_2\text{O}_3$ (JCPDS 33–0664) (Fig. 1d).

3.2. Comparison of O^* formation from water vs. CO_3^{2-} on the Fe_2O_3 catalyst

DFT calculations are employed to compare O^* formation from water vs. CO_3^{2-} on Fe_2O_3 . We employ an $\alpha\text{-Fe}_2\text{O}_3$ (0001) facet, which is considered an active surface in various electrochemical oxidation reactions [33–35]. We confirm that $\alpha\text{-Fe}_2\text{O}_3$ is the most stable phase under our experimental conditions ($\text{pH} = 10\text{--}12$, applied voltage of ~ 0.8 V vs. saturated calomel electrode (SCE) (V_{SCE})) based on a bulk Pourbaix diagram analysis [36,37].

The calculated free energy profile for the formation of O^* from water via the OER is presented in Fig. 2a. Among all the oxygen intermediates, i.e., OH^* , O^* and OOH^* , we consider O^* the active oxygen species for methane activation since the activation barrier for the OH^* -assisted route (1.2 eV) is approximately twice as high as that for the O^* -assisted route (0.6 eV). Notably, the $\text{OH}^* \rightarrow \text{O}^*$ step is the potential determining step, indicating that we cannot create O^* on $\alpha\text{-Fe}_2\text{O}_3$ (0001) via OER[38]. Applying the limiting potential of 2.0 V_{RHE} to promote the $\text{OH}^* \rightarrow \text{O}^*$ step makes the whole OER process exothermic; thus, the system rapidly generates O_2 , as shown in Fig. S3. The fast OER on $\alpha\text{-Fe}_2\text{O}_3$ (0001) indicates the poor utilization of O^* for methane activation. External oxidants inevitably generate O^* on $\alpha\text{-Fe}_2\text{O}_3$ (0001) during the electrochemical methane conversion process.

The calculated free energy profile for the formation of O^* from CO_3^{2-} is presented in Fig. 2b. Since it is difficult to directly calculate the energy of CO_3^{2-} solvated by water, we employ a thermodynamic cycle method (supplementary note #2) to indirectly obtain the energy. The electrochemical adsorption of CO_3^{2-} ($\text{CO}_3^{2-} \rightarrow \text{CO}_3^* + 2\text{e}^-$) is endothermic by 1.6 eV. However, if we assume that CO_3^* adsorption involves nearly a two-electron transfer reaction, the process becomes thermoneutral at 0.8 V_{RHE}. Under our experimental conditions for methane oxidation, i.e., 0.8 V_{SCE}, which is approximately 1.6 V_{RHE}, CO_3^* adsorption becomes exothermic by 0.8 eV. Once CO_3^* forms, it thermodynamically decomposes to O^* and CO_2 with a surmountable activation barrier of 0.8 eV. Notably, our experimental condition of 1.6 V_{RHE} for methane activation falls short of completely promoting the OER, in which the limiting potential is 2.0 V_{RHE}. This finding suggests that O^* that forms from CO_3^* does not oxidize to OOH^* and then O_2 gas; instead, it is utilized for O^* -assisted methane activation, as shown in Fig. 2a.

The formation of O^* from CO_3^{2-} on the Fe_2O_3 surface is confirmed experimentally. We analyze the gaseous product by applying an anodic

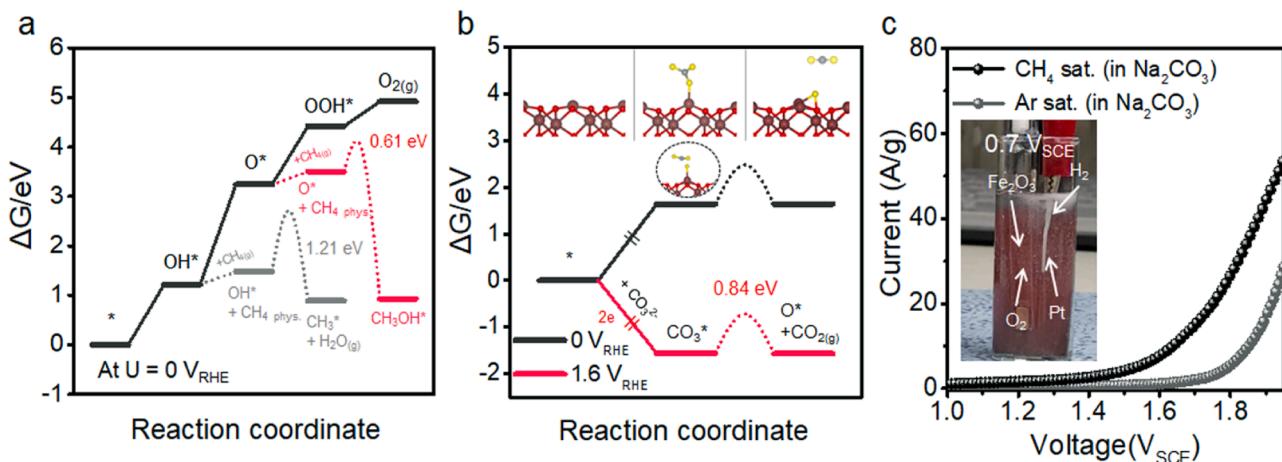


Fig. 2. DFT and LSV studies. (a) Free energy diagram for the OER on the Fe₂O₃ catalyst. Methane oxidation by O^{*}-assisted (red) and OH^{*}-assisted (gray) pathways are also displayed. (b) Free energy diagram for adsorption dissociation of CO₃²⁻ at potentials of 0 V_{RHE} and 0.8 V_{RHE}. The inset presents the atomic configuration for each reaction coordinate. The dark red, red/yellow, and gray spheres represent Fe, O, and C, respectively. The solid and dotted lines represent the electrochemical and thermodynamic routes, respectively. (c) LSV curves of Fe₂O₃ in CH₄-saturated and Ar-saturated electrolytes (control). (inset) Digital camera image of the three-electrode reactor at 1.6 V_{RHE}.

potential of 1.6 V_{RHE} to the Fe₂O₃ catalyst electrode in a methane-saturated CO₃²⁻ electrolyte. In situ mass spectrometry detects CO₂ (g) (Fig. S4); this CO₂ is released by the thermochemical dissociation of CO₃²⁻(CO₃²⁻ → CO₂ (g) + O^{*}), confirming the formation of O^{*}. The O 1s X-ray photoelectron spectroscopy (XPS) spectrum of the potential-applied Fe₂O₃ catalyst surface is presented (Fig. S5). The spectrum shows a high-intensity peak for the surface oxygen, confirming the presence of O^{*}[39,40].

Additionally, we analyze the linear sweep voltammetry (LSV) profile of the Fe₂O₃ catalyst in the electrolyte (Fig. 2c). The LSV curve exhibits a rapidly increasing oxidation current with an onset potential of approximately 1.6 V_{RHE}. This oxidation current is caused by water splitting; we observe the vigorous evolution of O₂ (g) and H₂ (g) on Fe₂O₃ and Pt electrode surfaces, respectively, at 2.4 V_{RHE} (Fig. S6). The LSV curve in the methane-saturated electrolyte exhibits a distinct profile from that in the bare electrolyte. The onset potential for the oxidation current exceeds the previous value of 1.0 V_{RHE}. This result reveals that methane oxidation proceeds prior to the OER on Fe₂O₃; at 1.6 V_{RHE}, little gas evolves at the Fe₂O₃ electrode, despite the evolution of H₂ at the Pt electrode (Fig. 2c); this phenomenon shows the production of water-soluble products (later identified as ethanol) by methane oxidation at the Fe₂O₃ electrode. The LSV analysis confirms a continuous production of stable O^{*} that drives the conversion of methane rather than the evolution into O₂.

3.3. Analysis of methane oxidation products and reaction pathways

We employ isotopically labeled CH₄ (¹³CH₄) and CO₃²⁻ (¹⁸O₃²⁻) to identify products in electrochemical methane conversion on the Fe₂O₃ catalyst. The carbon-13 nuclear magnetic resonance (¹³C NMR) spectrum for the liquid-phase product is shown in Fig. 3a. We identify ethanol as the major product, and all carbon atoms are labeled ¹³C; small amounts of methanol and acetone with ¹³C are identified. The gas chromatography—mass spectrometry (GC—MS) spectrum for ethanol is presented in Fig. 3b. In addition to the peaks assigned to ¹⁶O ethanol, we observe peaks shifted by 2 m/z, which correspond to ¹⁸O-containing ethanol. The intensity of the shifted peak is approximately 40 % of the ¹⁶O ethanol peak intensity. This ratio corresponds to the ratio of C¹⁶O₃²⁻:C¹⁸O₃²⁻ used in the reaction, indicating that there is CO₃²⁻ is the only oxygen source. The isotope reaction identifies the conversion of methane to alcohol by the oxygen from CO₃²⁻.

The productivities for methane conversion at various applied

voltages are compared, as shown in Fig. 3c (Table 1). Under all conditions, ethanol is the main product among oxygenates. Ethanol production increases to 1.6 V_{RHE}. However, at high applied voltages, ethanol production decreases. This phenomenon corresponds to a decrease in methane conversion productivity as O^{*} is consumed in the OER. In the LSV profile, the oxidation current for the OER rapidly increases from 1.6 V_{RHE}. The production rate is the highest at 1.6 V_{RHE}, achieving 1198.3 μmol/g_{cat}/hr with 86 % selectivity; the FE for total oxygenates is 87 %. The maximum production rate surpasses those of previous electrocatalysts, including CuO/CeO₂ (1009.8 μmol/g_{cat}/hr for methanol), Rh/ZnO (789 μmol/g_{cat}/hr) and NiO/Ni (25 μmol/g_{cat}/hr) (see Table S1). The selectivity is the highest at 1.6 V_{RHE}. Based on this voltage, the ethanol selectivity decreases with the production of methanol in the low-voltage region and the production of acetone in the high-voltage region (Fig. 3d).

DFT calculations are employed to identify the minimum free-energy pathway for methane-to-ethanol conversion on O^{*}/Fe₂O₃; the results are shown in Fig. 3e. The pathway starts by activating methane on O^{*} produced via the thermochemical dissociation of carbonate ions that are electrochemically adsorbed on Fe₂O₃. That is, the C—H bond of methane is cleaved while forming a C—O bond to directly produce CH₃OH^{*}(CH₄ + O^{*} → CH₃OH^{*}, ΔG = -2.6 eV with a low free-energy barrier of 0.6 eV). This O^{*}-assisted methane activation route is thermodynamically preferred to that producing CH₃^{*} and OH^{*}(CH₄ + O^{*} → CH₃^{*} + OH^{*}[41], ΔG = -1.6 eV with a low free-energy barrier of 0.6 eV); nevertheless, both reactions are highly exothermic. Then, CH₃OH^{*} deprotonation occurs via the cleavage of the C—H bond to produce CH₂OH^{*}, as the cleavage of the O—H bond to produce CH₃O^{*} is more endothermic by 2 eV [41–43]. Since CH₂OH^{*} deprotonation is an electrochemical reaction (CH₂OH^{*} → CH₂OH^{*}+ H⁺ + e⁻), it becomes highly exothermic under an applied potential of 1.6 V_{RHE}, surpassing the competition with CH₃OH^{*} desorption to form methanol (CH₃OH^{*} → CH₃OH, ΔG = 0.3 eV). These results are in agreement with the experimental finding that more ethanol is produced than methanol, particularly at high anodic potentials.

Since CH₂OH^{*}, which has a strong polarity of carbonyl oxygen, is susceptible to nucleophilic attacks, direct bonding between CH₂OH^{*} and CH₃^{*} is presumed for ethanol synthesis[44]. Since CH₄ + O^{*} → CH₃^{*} + OH^{*} is exothermic, CH₃^{*} may form on the catalyst surface. Fig. S7 shows the calculated free energy profile for ethanol production via the coupling of CH₂OH^{*} and CH₃^{*}. While this route seems possible with the highest free energy barrier of approximately 0.8 eV, it leads to

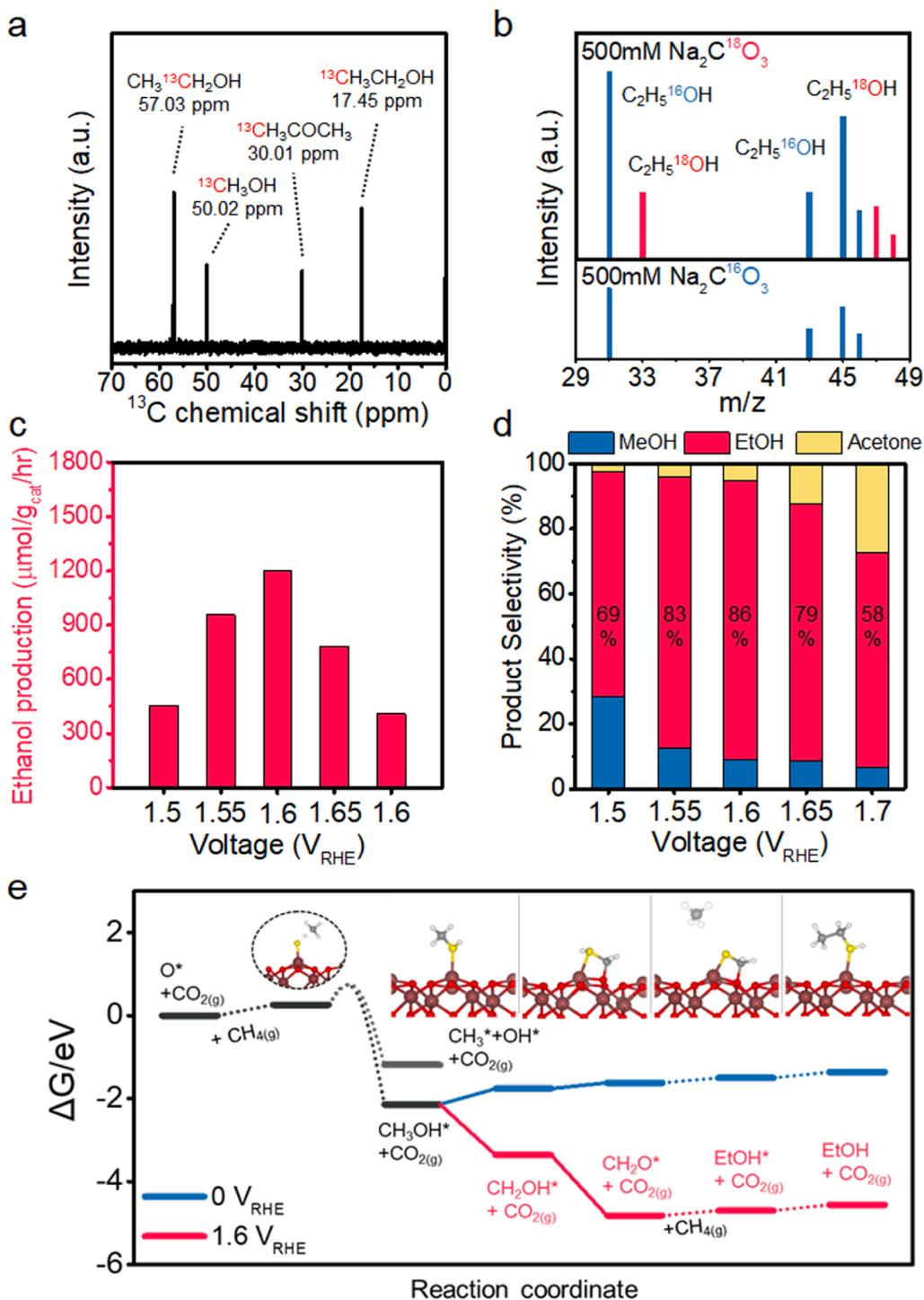


Fig. 3. Electrochemical methane–ethanol conversion. (a) ¹³C NMR spectrum of the product reacted using ¹³CH₄. (b) GC-MS spectrum for ethanol of the product reacted using C¹⁸O₃⁻. (c) Ethanol production at various applied voltages. (d) Selectivity for the main oxygenates at various applied voltages. (e) Calculated free energy diagrams for methane–ethanol conversion at 0 V_{RHE} and 1.6 V_{RHE}. The cartoons are atomic configurations corresponding to each reaction coordinate. The solid and dashed lines represent the electrochemical and thermochemical steps, respectively.

the formation of OH* (CH₄ + O* → CH₃*+OH*) that is difficult to remove from the catalyst surface via OER. If we apply the limiting potential for the OER (2.0 V_{RHE}) to oxidize OH* to oxygen gas, O* formed from CO₃²⁻ oxidizes to oxygen gas. Thus, ethanol production via the coupling of CH₂OH* and CH₃* is not feasible on α-Fe₂O₃ (0001). CH₂OH* must be further deprotonated to CH₂O*, which is highly exothermic under an applied potential of 1.6 V_{RHE}; then, it must combine with CH₄, as shown in Fig. 3e.

The reaction of CH₂O* with CH₄ to form EtOH* is thermochemical, and the reaction free energy is near thermoneutral; this observation indicates that ethanol production via the coupling of CH₂O* and CH₄ is thermodynamically possible under ambient conditions. The transition state for this reaction step (CH₂O* + CH₄ → EtOH*) resembles a methyl radical interacting with CH₂OH*, in which the energy cannot be calculated accurately, as explicitly modeling the solvation of the methyl radical in water is extremely difficult. However, since no other C–C

Table 1

Comparison of catalytic activity for the liquid phase oxidation of CH₄ using Na₂CO₃. Test condition: catalyst: Fe₂O₃ / Zr-doped Fe₂O₃, Reaction temperature = 298 K, electrolyte = 0.5 M Na₂CO₃, CH₄ pressure = 1 bar, Reaction Time = 1 h.

Entry	Catalyst	Voltage (V _{RHE})	Amount of product ($\mu\text{mol/g}_{\text{cat}}$) (Selectivity)		
			Ethanol	Methanol	Acetone
1	Fe ₂ O ₃	1.5	456 (69.4 %)	185 (28.2 %)	15.3 (2.3 %)
2	Fe ₂ O ₃	1.55	957 (83.5 %)	144 (12.5 %)	45.3 (4.0 %)
3	Fe ₂ O ₃	1.6	1198 (86.1 %)	124 (8.9 %)	70.0 (5.0 %)
4	Fe ₂ O ₃	1.65	783 (79.1 %)	84.6 (8.5 %)	127 (12.4 %)
5	Fe ₂ O ₃	1.7	408 (66.1 %)	40.0 (6.5 %)	169 (27.5 %)
6	0.01 wt% Zr-doped Fe ₂ O ₃	1.6	1369 (88.5 %)	107 (6.9 %)	70.1 (4.5 %)
7	0.05 wt% Zr-doped Fe ₂ O ₃	1.6	1677 (90.5 %)	82.6 (4.3 %)	99.2 (5.2 %)
8	0.1 wt% Zr-doped Fe ₂ O ₃	1.6	1549 (89.8 %)	60.1 (3.5 %)	116 (6.7 %)

bonding routes to form ethanol are possible (once CH₂O* is further deprotonated to CHO*, there is no pathway to produce ethanol without undergoing reduction (protonation) steps under oxidizing (anodic) conditions in principle), we carefully argue that this is the most feasible route for producing EtOH* on O*/Fe₂O₃. Finally, although the desorption of EtOH* to EtOH (g) is slightly endothermic with a reaction free energy of 0.1 eV, ethanol production in an aqueous environment is likely to be spontaneous; this spontaneity occurs since EtOH_(aq) is much lower in energy than EtOH (g) due to hydrogen bonding with the water solvent, and desorption reactions are usually barrierless.

DFT calculations are performed to examine the possibility of the deeper oxidation of ethanol to acetone on the Fe₂O₃ surface. Although the electrochemical barriers are not calculated, ethanol deprotonations occur via EtOH* → CH₃CHOH* → CH₃CHO* → CH₃CO*. Once CH₃CO* forms, further deprotonation is extremely endothermic; thus, it reacts with CH₃* produced via CH₄ + O* → CH₃* + OH*. This CH₃CO* -CH₃* coupling reaction directly forms acetone on the surface, in which the desorption is moderately uphill (0.7 eV) in free energy. Although acetone production initially appears to be feasible, for a complete catalytic cycle (stable acetone production), OH* produced via CH₄ + O* → CH₃* + OH* must be removed as O₂ via the OER, in which the limiting potential is very high (2.0 V_{RHE}), as discussed above. Even if an anodic potential higher than 2.0 V_{RHE} is applied, acetone production is unlikely to dominate, as O* is oxidized to O₂ and not much O* is available for methane activation. These results are in agreement with the experimental finding that little acetone is produced, particularly at low anodic potentials.

3.4. Improvement of ethanol productivity by Zr doping

Since the key to increasing the ethanol selectivity is to stabilize CH₂OH* relative to CH₃OH (g), we first theoretically devise a Zr-doping strategy to increase the oxophilicity of the Fe₂O₃ surface to achieve high ethanol selectivity (note that CH₂OH* binds to the surface through oxygen) [33,45]. Fig. S10 shows the calculated Pourbaix diagram for the Zr-doped α -Fe₂O₃ (0001) surface. Unlike the pristine Fe₂O₃ surface, OH* is strongly preadsorbed on the Zr site of the Zr-doped Fe₂O₃ surface even under weakly oxidizing conditions. Fig. 4a shows the changes in the free energy diagram for the methane to ethanol conversion when Zr is doped to the α -Fe₂O₃ (0001) surface and OH* is preadsorbed on the Zr site.

Only the intermediates containing -OH groups, such as CH₃OH*, CH₂OH* and EtOH*, are stabilized by 0.1 eV, thermodynamically promoting the ethanol production pathway over methanol. The selective stabilization is attributed to the formation of the hydrogen bond between the -OH group of the intermediate and the preadsorbed OH* (Fig. S11)[46]. Notably, the RPBE functional is used for all these calculations. By using a functional that accurately accounts for dispersion interactions, greater extents of stabilization are to be expected [47,48].

To experimentally verify the strategy for improving the ethanol selectivity, we prepare a Zr-doped Fe₂O₃ catalyst by coprecipitation with a precursor of zirconium(IV) oxynitrate. We control the concentration of the Zr precursor to obtain Fe₂O₃ catalysts containing 0.01, 0.05 and 0.1 wt% Zr. The Zr-doped Fe₂O₃ particles exhibit sizes of 50–300 nm, similar to those of conventional Fe₂O₃ particles (Fig. 4b). The elemental analysis shows a uniform distribution of Zr (Fig. 4c and Fig. S12). The XRD peaks of Zr-doped Fe₂O₃ are similar to those of Fe₂O₃. However, the peaks of Zr-doped Fe₂O₃ are shifted to smaller angles than the peaks of bare Fe₂O₃; this shift is attributed to the expansion of the crystal lattice induced by the incorporation of Zr, in which the atomic radius is approximately twice that of Fe. The peaks corresponding to ZrO₂ are not observed (Fig. 4d).

The ethanol productivity and selectivity on the Fe₂O₃ catalysts with various Zr contents are presented in Figs. 4e and 4f, respectively (Table 1). We achieve the maximum production rate at 0.05 wt% Zr. The low production rate at 0.1 wt% Zr is rationalized by a decrease in conductivity due to lattice distortion caused by Zr doping. Electrochemical impedance spectroscopy is applied to compare the charge transfer resistivity at various doping contents; the lowest resistivity appears at 0.05 wt%, and the resistivity increases at 0.1 wt% (Fig. S13). The ethanol production rate reaches 1677 $\mu\text{mol/g}_{\text{cat}}/\text{hr}$ at 1.6 V_{RHE}, which is a 53 % improvement compared to the bare Fe₂O₃ catalyst. The ethanol productivity of 0.05 wt% Zr-doped Fe₂O₃ at various applied potentials, similar to that of bare Fe₂O₃, exhibits a maximum at 1.6 V_{RHE} and decreases at potentials above this (Fig. S14); the optimum potential coincides with that for the bare Fe₂O₃ catalyst. Zr doping improves the ethanol selectivity; the selectivity under 0.05 wt% Zr doping reaches 91 %. The conversion of the 0.05 wt% Zr-doped Fe₂O₃ catalyst is superior to the results of the previous liquid-phase methane–methanol (or ethanol) catalytic conversion (see Table S1). More impressively, the Zr-doped Fe₂O₃ catalyst exhibits high selectivity even at high ethanol production rates (see Fig. S15). We confirm the long-term stability of the electrochemical conversion with the Zr-doped Fe₂O₃ catalyst (Fig. 4g). The 0.05 wt% Zr-doped Fe₂O₃ catalyst exhibits stable operation with only a 10 % reduction in the oxidation current for 18 h. The areal oxidation current values are high compared to those of recent catalysts applied to electrochemical methane conversion (Table S2). After the reaction, the Zr-doped Fe₂O₃ retains the XRD pattern corresponding to α -Fe₂O₃ (Fig. S16). The TEM image exhibits the same size and polyhedral morphology as before the reaction (Fig. S16).

4. Conclusion

We demonstrate electrochemical methane–ethanol conversion by employing Fe₂O₃ catalysts with CO₃²⁻ oxygen source. The free-energy profile for the OER on α -Fe₂O₃ (0001) shows difficulties in maintaining active O* on the catalyst surface due to the second step of the OER (OH* → O*) being the potential determining step. In contrast, the CO₃²⁻ oxygen source generates O* via thermochemical dissociation, ensuring stable formation of O* in a potential range that is not sufficient to promote the OER. We obtain methane conversion productivity that increases with increasing potential in the range of 0.8–1.6 V_{RHE}; however, at higher potentials, the productivity is reduced due to the activation of the OER. The electrochemical methane oxidation on the O-promoted Fe₂O₃ catalyst produces mainly ethanol. DFT calculations show that the ethanol production route consists of O*-induced methane activation, CH₃OH* deprotonation, and then coupling of CH₂O* with methane. On

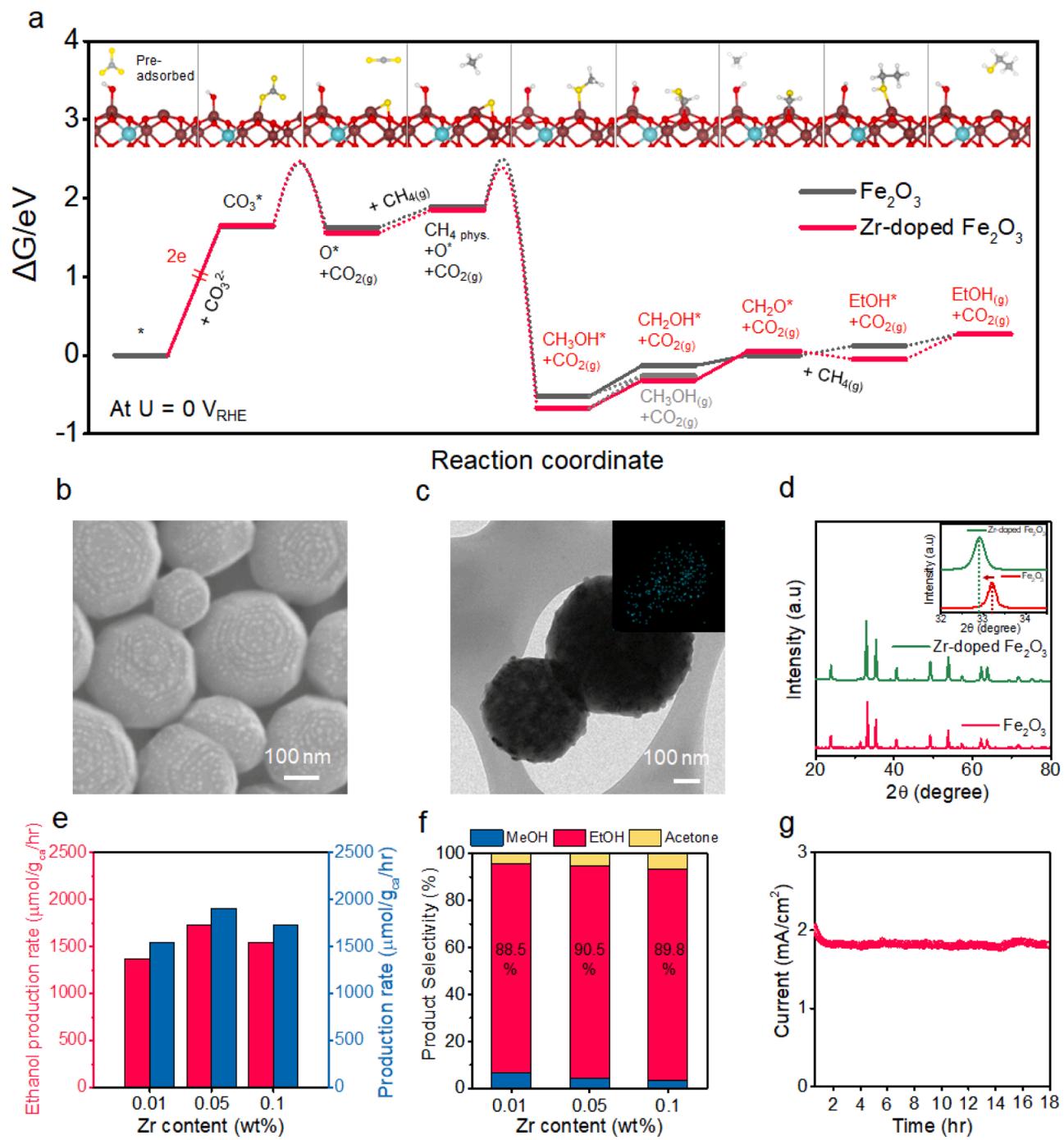


Fig. 4. Effect of Zr doping. (a) Calculated free energy diagrams for O* production and methane–ethanol conversion on the Zr-doped Fe₂O₃ catalyst. The energy profile of Fe₂O₃ is presented for comparison. The cartoons are atomic configurations corresponding to each reaction coordinate. The solid and dashed lines represent the electrochemical and thermochemical steps, respectively. (b) SEM and (c) TEM/EDS images and (d) XRD spectra of the Zr-doped Fe₂O₃ catalyst. The inset of Fig. 4d shows the peaks corresponding to the (104) plane of Zr-doped Fe₂O₃ and Fe₂O₃. (e) Production rates of ethanol and total oxygenates and (f) selectivity for major products with varying Zr content. The applied voltage is 1.6 V_{RHE}. (g) Areal current density at 1.6 V_{RHE} for electrochemical methane oxidation on Zr-doped Fe₂O₃ nanoparticles as a function of reaction time.

the Fe₂O₃ surface, CH₃OH* deprotonation is thermodynamically preferred to CH₃OH* desorption, leading to high ethanol selectivity. To further enhance the methane–ethanol conversion, Zr doping is applied. Mechanistic studies show that the Zr dopant allows the formation of OH* that stabilizes only the intermediates that contain the –OH group via hydrogen bonding. We achieve an ethanol production rate of 1198.3 $\mu\text{mol/g}_{\text{cat}}/\text{hr}$ with a selectivity of 86 % over the Fe₂O₃ catalyst. The 0.05 wt% Zr-doped Fe₂O₃ catalyst achieves a 53 % improvement in the production rate to 1677 $\mu\text{mol/g}_{\text{cat}}/\text{hr}$ (the total production rate for

oxygenates is 1831 $\mu\text{mol/g}_{\text{cat}}/\text{hr}$ over bare Fe₂O₃, where the ethanol selectivity is 91 %. The FE for oxygenates on these Fe₂O₃ catalysts reaches 87 %. This achievement with these Fe₂O₃ catalysts with CO₃²⁻ is outstanding compared to the liquid-phase methane–alcohol conversion obtained with various advanced catalysts. Our work presents an understanding and achievement of electrochemical methane conversion under ambient conditions. Moreover, this study sheds light on the direction in which electrochemical catalyst systems are headed for partial oxidation of methane to alcohols.

CRediT authorship contribution statement

Jaehyun Lee: Investigation, Formal analysis, Data curation. **Sungwoo Lee:** Theoretical simulation, Formal analysis, Data curation. **Cheolho Kim:** Data curation. **Jong Suk Yoo:** Conceptualization, Supervision, Writing - original draft, Writing – Review & Editing. **Jun Hyuk Moon:** Conceptualization, Funding acquisition, Supervision, Project administration, Writing - original draft, Writing – Review & Editing.

Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

Data Availability

Data will be made available on request.

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Appendix A. Supporting information

Supplementary data associated with this article can be found in the online version at [doi:10.1016/j.apcatb.2023.123633](https://doi.org/10.1016/j.apcatb.2023.123633).

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